

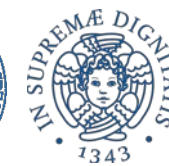
BHETSA Status

Novel prototype filter for the ET Superattenuator

A. Allocca, S. Ardito, M. Baratti, G. Bartoli, L. Bellizzi, S. Bianchi, V. Boschi, E. Calloni, M. Carpinelli, P. Chessa, D. D'Urso, R. De Rosa, L. Di Fiore, F. Fabrizi, I. Ferrante, F. Fidecaro, A. Fiori, A. Gennai, A. Longo, M. Montani, L. Papalini, M. Palaia, M. Razzano, D. Rozza, P. Ruggi, L. Trozzo, M. Vacatello, A. Viceré

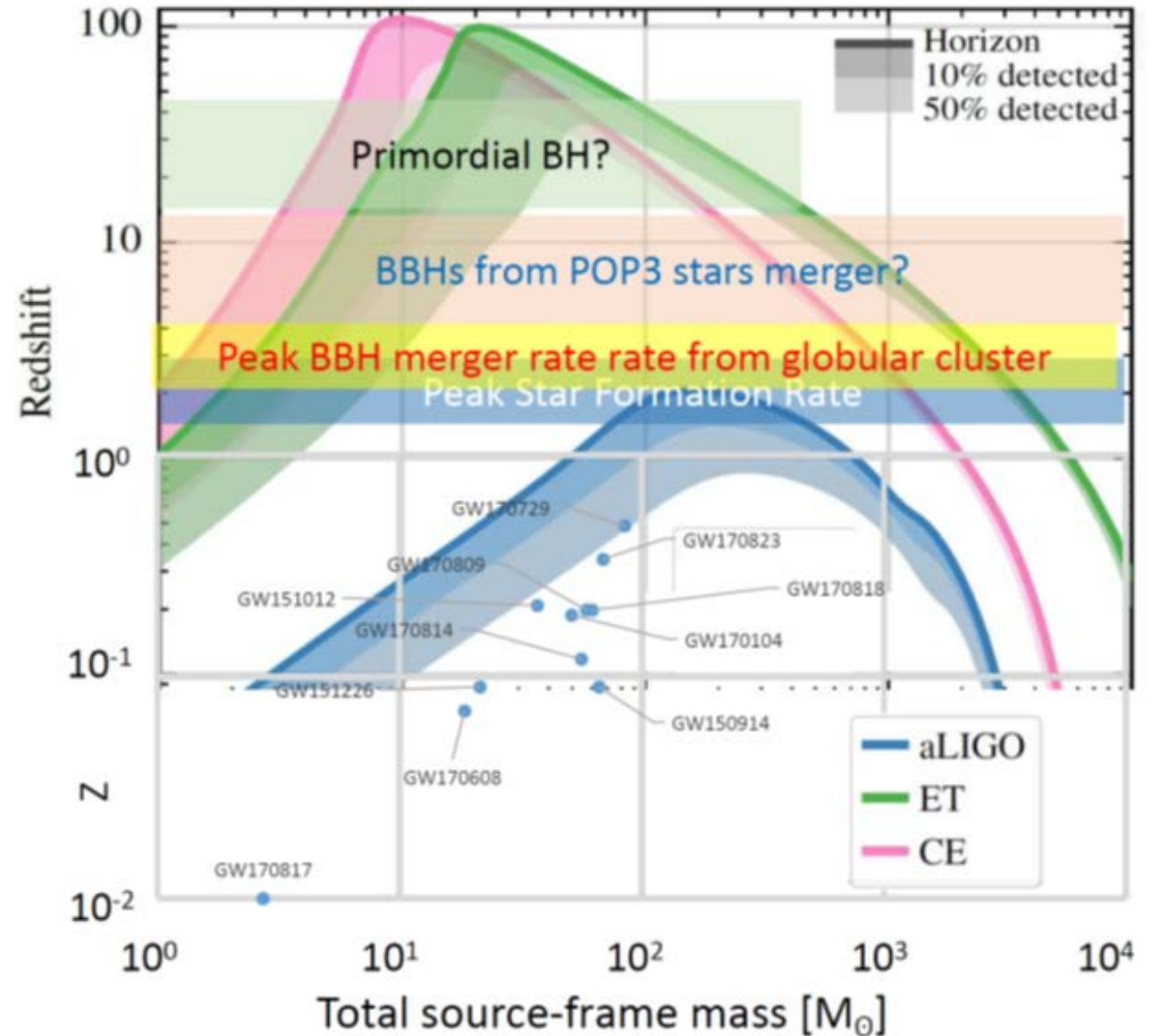
INFN – Na, INFN – Pi, Uni Napoli, Uni Pisa, Uni Sassari, Uni Urbino

BHETSA PRIN Meeting, Urbino, November 24, 2023

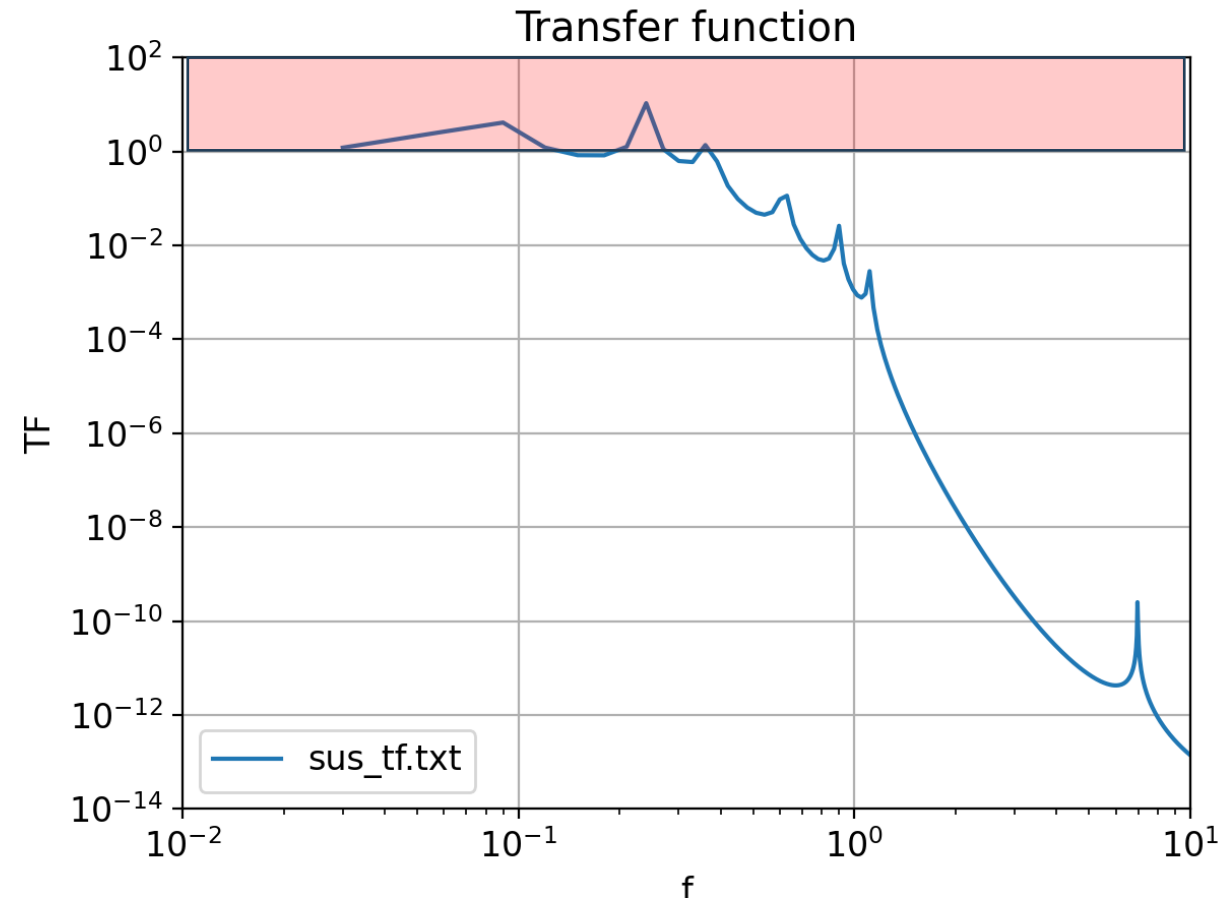


Sensitivity to low frequency:

- Higher system total mass
- Higher signal red shift, earlier in Universe history
- Earlier presence of signal in the detection band, earlier warning



- Ground motion $10^{-7} \text{ m Hz}^{-1/2}$ at 1 Hz vs $10^{-18} \text{ m Hz}^{-1/2}$ at 10 Hz
- Test mass asks for a very loose link
 - Low pass filter with a steep frequency cut below the detection band
 - Cascade of harmonic oscillators (Second Order Sections)
 - Loose springs and high masses
- Dissipation to be avoided, not compatible with loose link
- Loose link through local active control limited by sensor noise
- Passive isolation for a large fraction of the chain
- But amplification at normal modes



ET-LF requirements

LF noise is given by

- Microseism motion
- Newtonian noise
- Upconversion of residual motion into the detection band
- Control noise

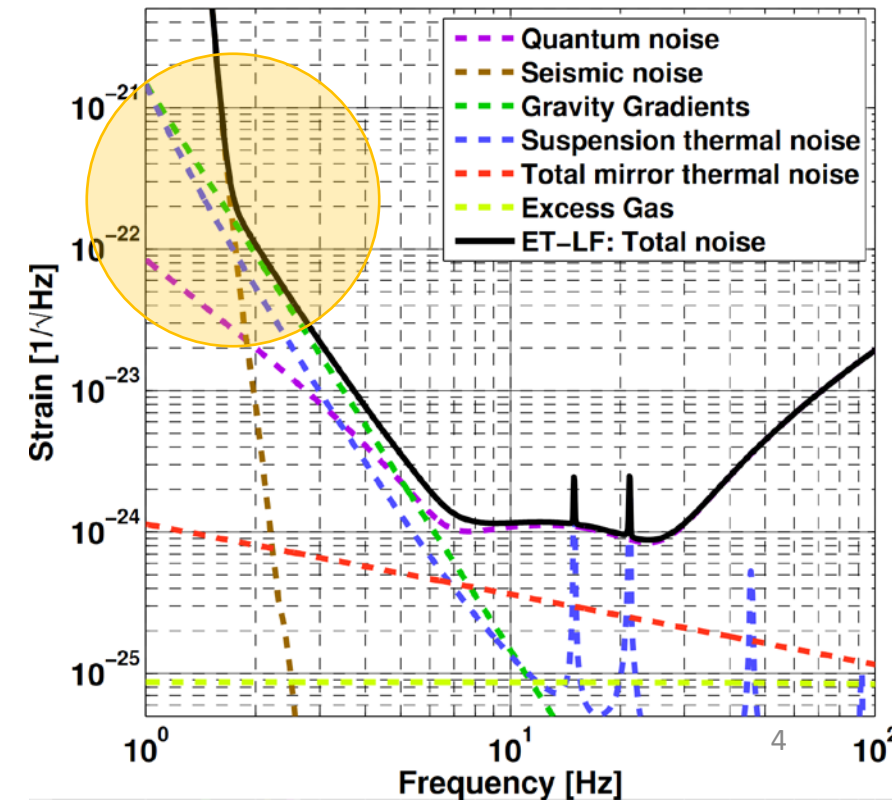
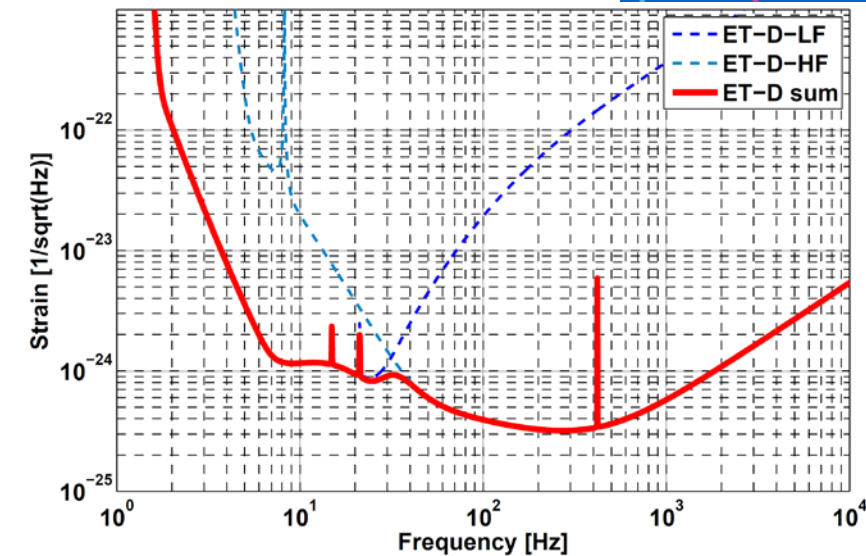
Design curve based on 17 m tall suspensions

Reduction to less than 10 m:

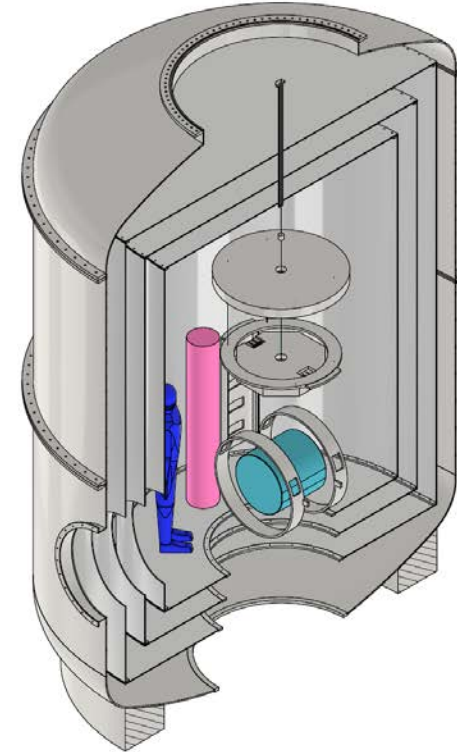
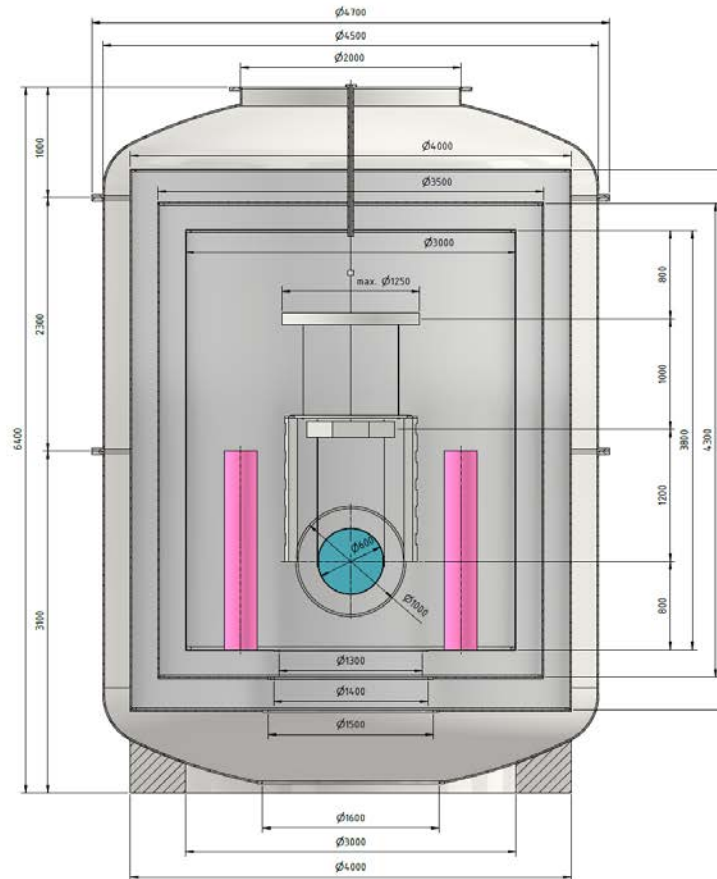
- Significantly lower cavern excavation cost
- Suspension management similar to Virgo

Newtonian noise crossing:

$2 \cdot 10^{-22} \text{ Hz}^{-1/2}$ at 1.8 Hz (AdV: 3.2 Hz)



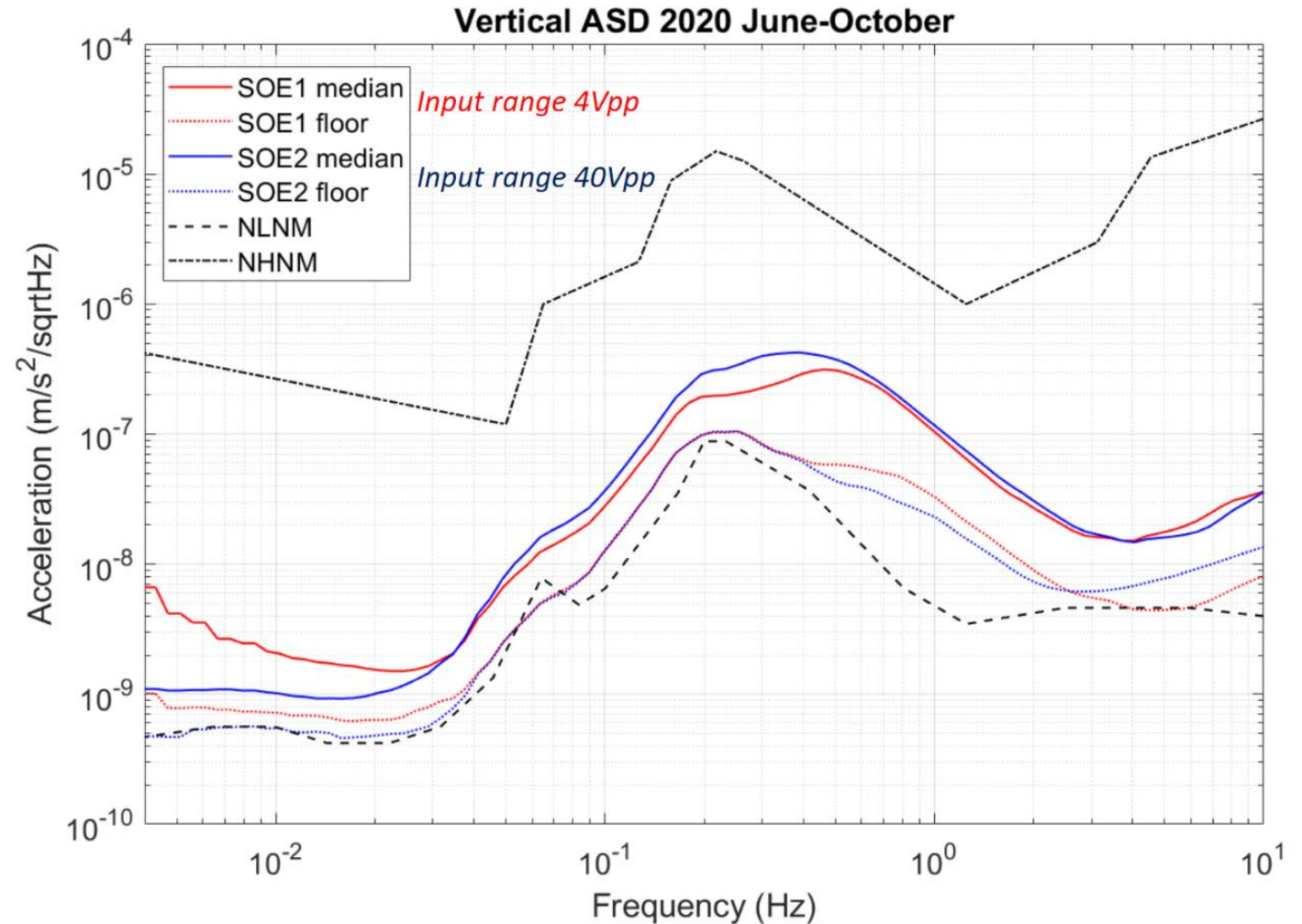
1. Act on ground / suspension interface actively
2. Act on suspension point actively/passively
3. Superattenuator chain design
4. Payload design compatibility: large occupancy announced ϕ 4700 h 6400



Sardinia vertical

$3 \cdot 10^{-8} \text{ ms}^{-2} \text{ Hz}^{-1/2}$ at 2 Hz

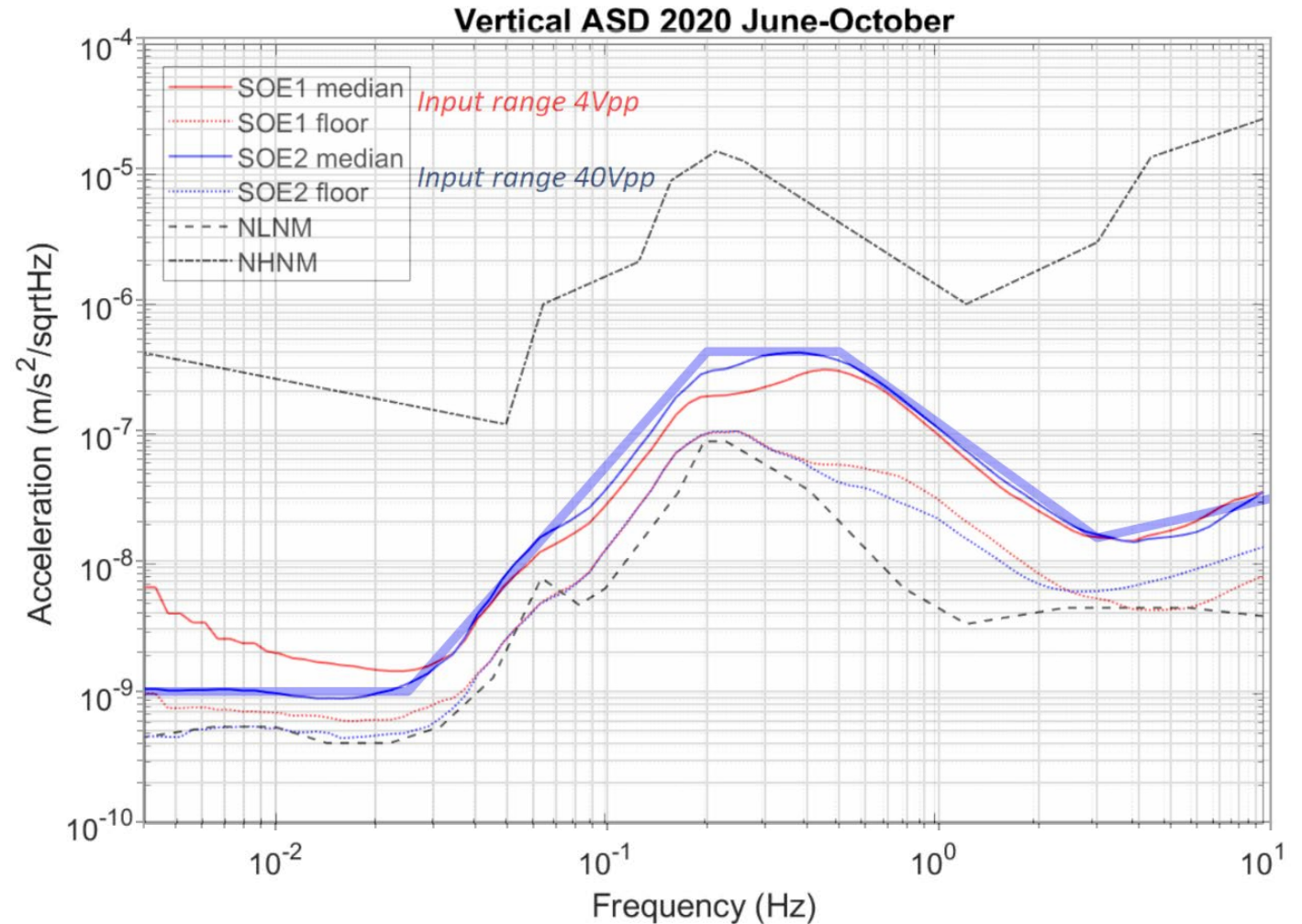
To be updated with
borehole measurements
at Sos Enattos (L.
Naticchioni)



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Vertical displacement spectrum

Virgo: $5 \cdot 10^{-10} \text{ m Hz}^{-1/2}$ at 10 Hz

SOE: $3 \cdot 10^{-10} \text{ m Hz}^{-1/2}$ at 2 Hz

RMS displacement over 100 s

Virgo: 10^{-6} m comparable to λ

SOE: 10^{-7} m well below λ

Strain

Virgo: $2 \cdot 10^{-22} \text{ Hz}^{-1/2}$ at 10 Hz

ET: $2 \cdot 10^{-22} \text{ Hz}^{-1/2}$ at 2 Hz

Four uncorrelated mirrors

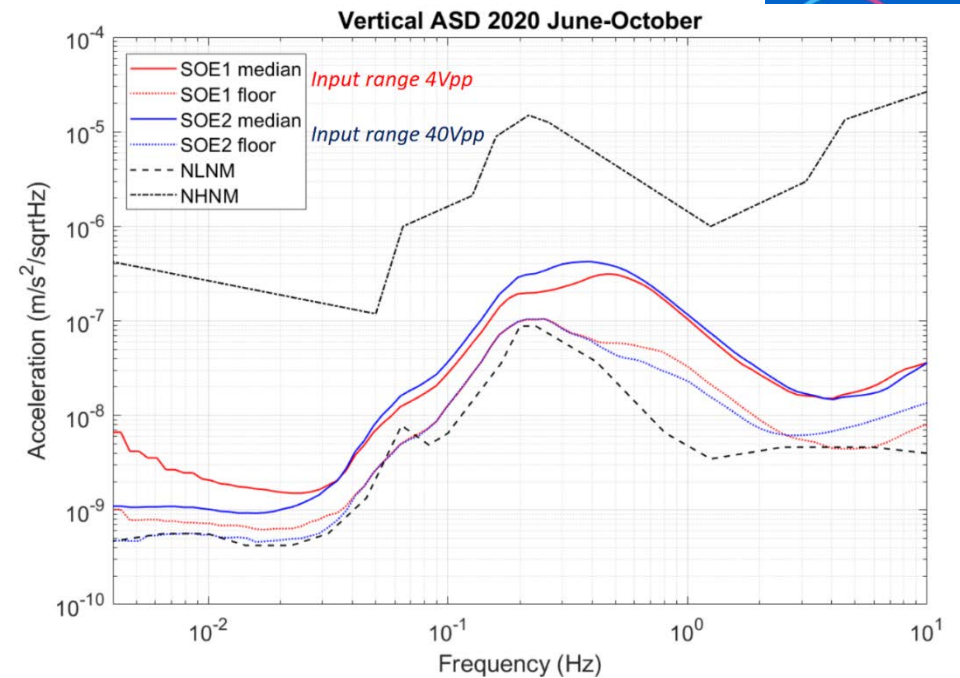
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With factor 10 safety factor

Virgo: $1.5 \cdot 10^{-19} \text{ m Hz}^{-1/2}$ at 10 Hz

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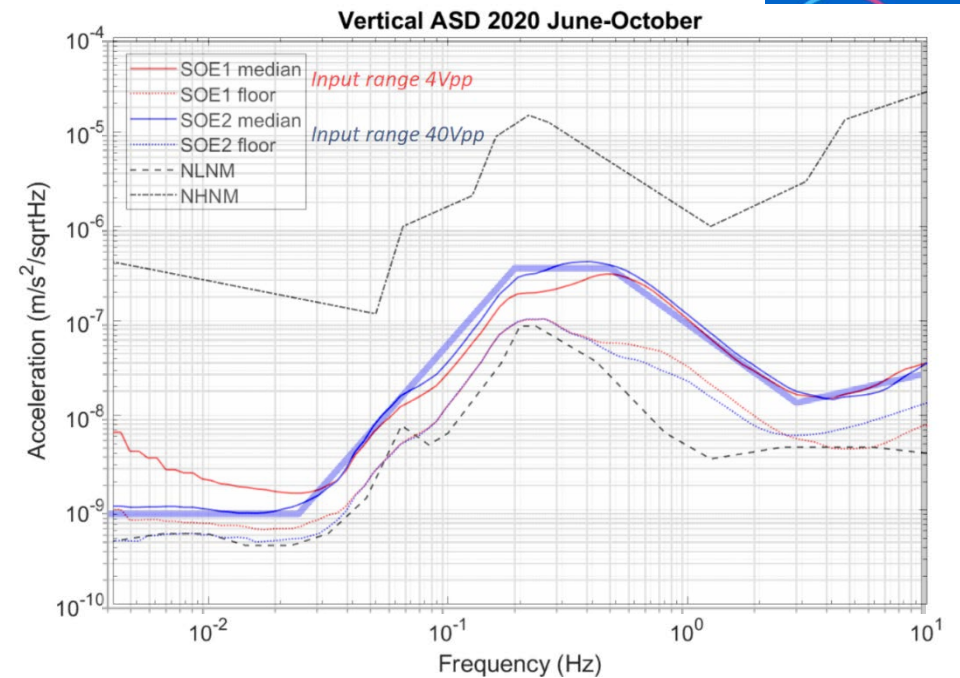
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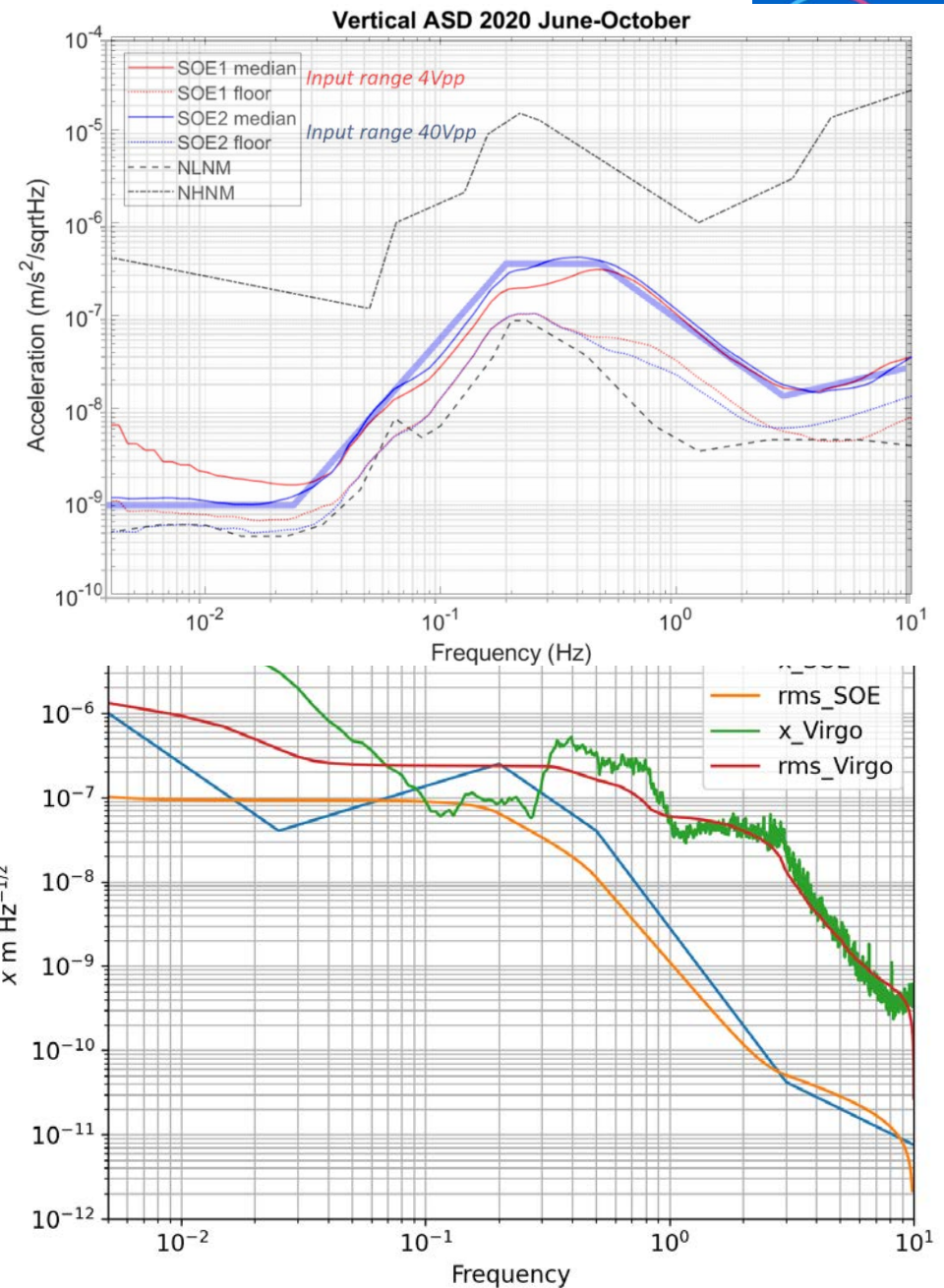
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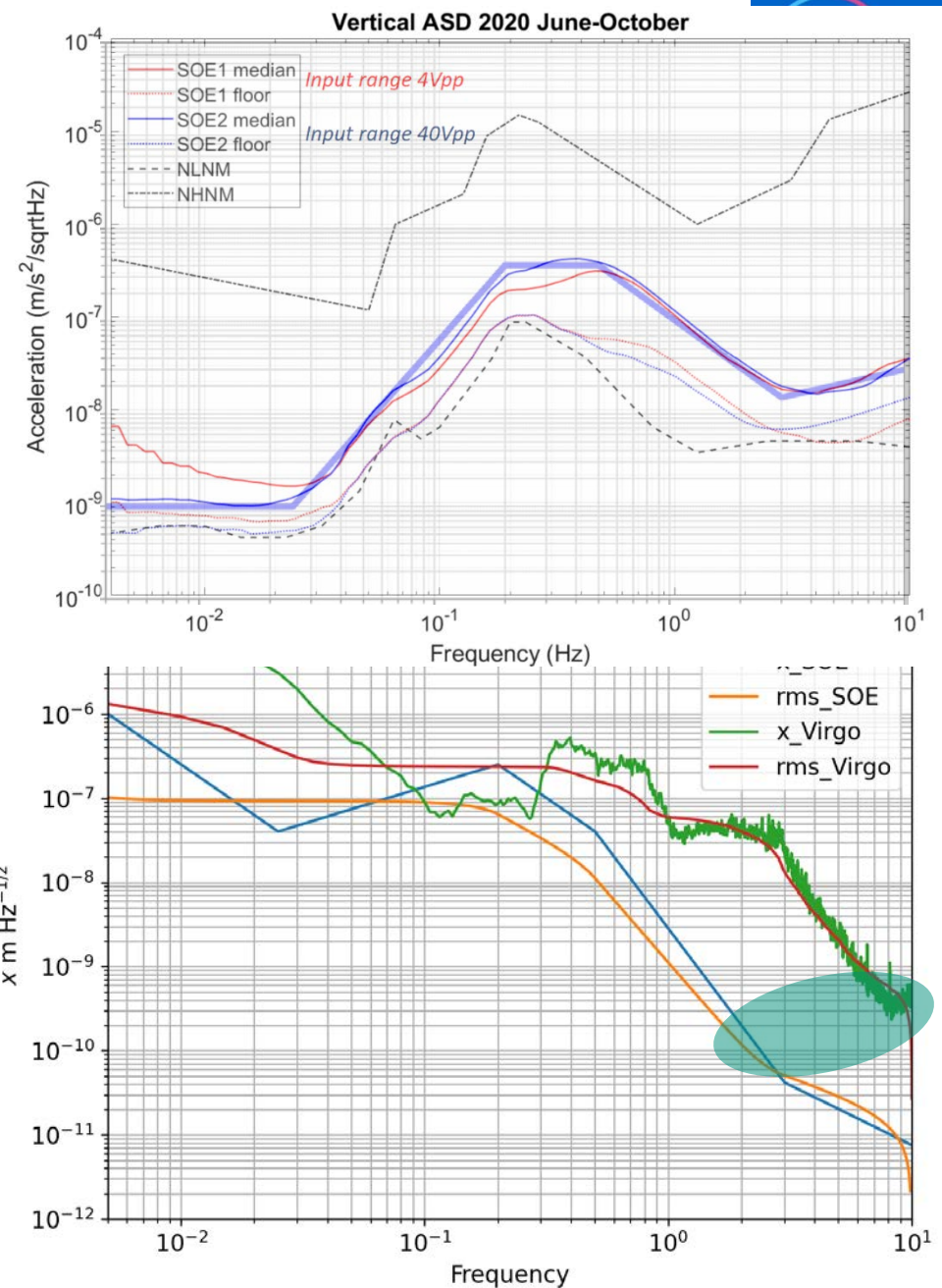
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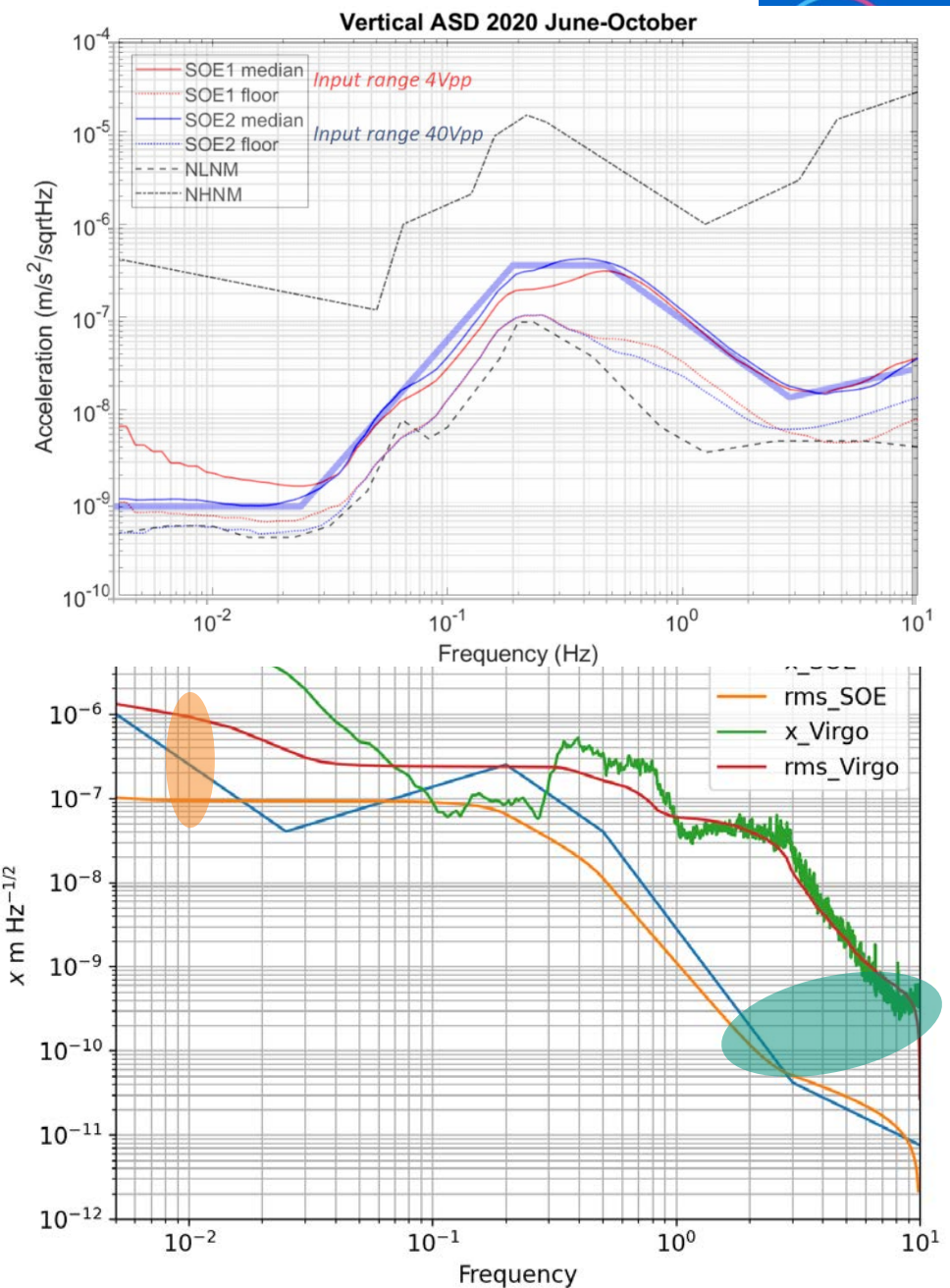
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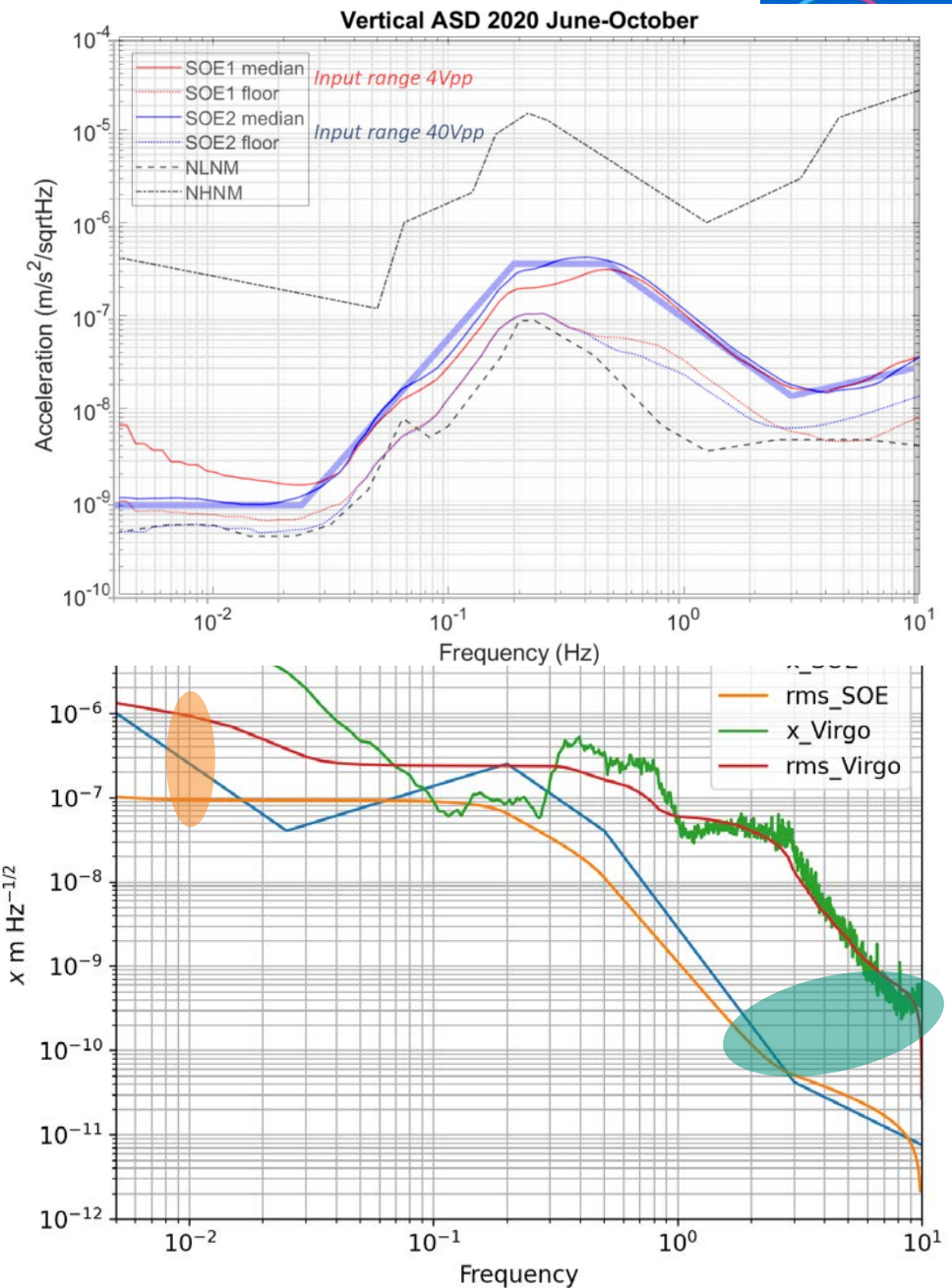
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Einstein Telescope

Vertical displacement spectrum

SOE: $3 \cdot 10^{-10} \text{ m Hz}^{-1/2}$ at 2 Hz

30 mHz Inverted pendulum

Attenuation at 2 Hz: $2.3 \cdot 10^{-4}$

Motion at 2 Hz: $7 \cdot 10^{-14} \text{ m Hz}^{-1/2}$

Noise floor for local sensing

Virgo

Vertical displacement spectrum

Virgo: $5 \cdot 10^{-10} \text{ m Hz}^{-1/2}$ at 10 Hz

30 mHz Inverted pendulum

Attenuation at 10 Hz: $9 \cdot 10^{-6}$

Motion at 10 Hz: $5 \cdot 10^{-15} \text{ m Hz}^{-1/2}$

Beyond noise floor for local sensing

Einstein Telescope

Vertical displacement spectrum

SOE: $3 \cdot 10^{-10} \text{ m Hz}^{-1/2}$ at 2 Hz

30 mHz Inverted pendulum

Attenuation at 2 Hz: $2.3 \cdot 10^{-4}$

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Noise floor for local sensing

With factor 10 safety factor

ET: $10^{-19} \text{ m Hz}^{-1/2}$ at 2 Hz

Full seismic attenuation required

ET: $1.5 \cdot 10^{-6}$ at 2 Hz

Virgo

Vertical displacement spectrum

Virgo: $5 \cdot 10^{-10} \text{ m Hz}^{-1/2}$ at 10 Hz

30 mHz Inverted pendulum

Attenuation at 10 Hz: $9 \cdot 10^{-6}$

Motion at 10 Hz: $5 \cdot 10^{-15} \text{ m Hz}^{-1/2}$

Beyond noise floor for local sensing

With factor 10 safety factor

Virgo: $1.5 \cdot 10^{-19} \text{ m Hz}^{-1/2}$ at 10 Hz

Full seismic attenuation required

Virgo: $A = 3 \cdot 10^{-5}$ at 10 Hz

Einstein Telescope

Full seismic attenuation required

ET: $1.5 \cdot 10^{-6}$ at 2 Hz

Mandatory filters

Mirror: pendulum at 0.46 Hz

Marionetta

Assume 2 filters mode at 0.75 Hz:

$A = 2.7 \cdot 10^{-2}$ at 2 Hz

Remaining attenuation required

$A_{\text{ch}} = 5.6 \cdot 10^{-5}$ at 2 Hz

Virgo

Full seismic attenuation required

Virgo: $A = 3 \cdot 10^{-5}$ at 10 Hz

Mandatory filters

Mirror: pendulum at 0.6 Hz

Marionetta

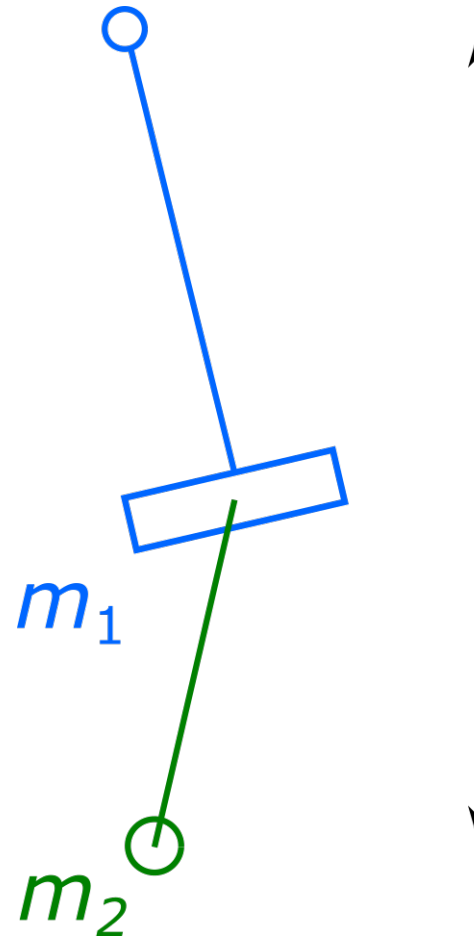
Assume 2 filters mode at 0.75 Hz:

$A = 5.6 \cdot 10^{-3}$ at 10 Hz

Remaining attenuation required

$A_{\text{ch}} = 5.4 \cdot 10^{-3}$ at 10 Hz

Cascade of pendulums
Using inertia and gravity

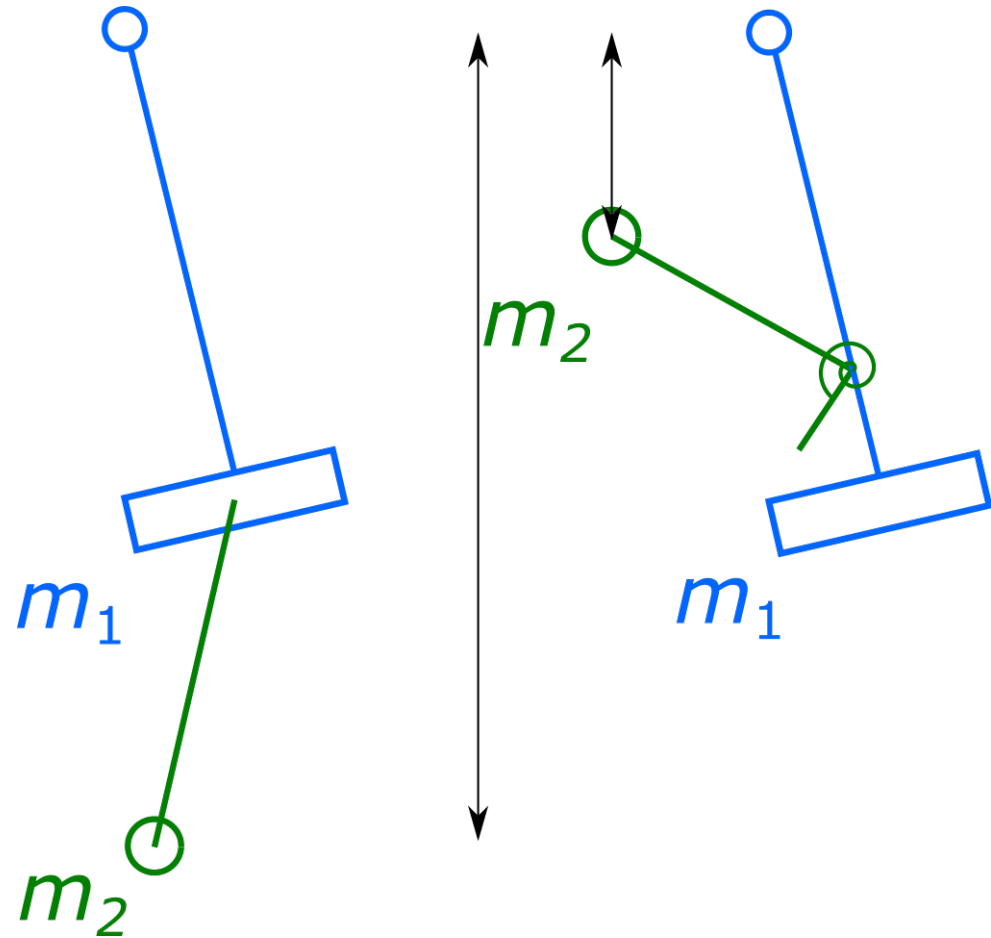


Cascade of pendulums

Using inertia and gravity

To using inertia, springs and gravity

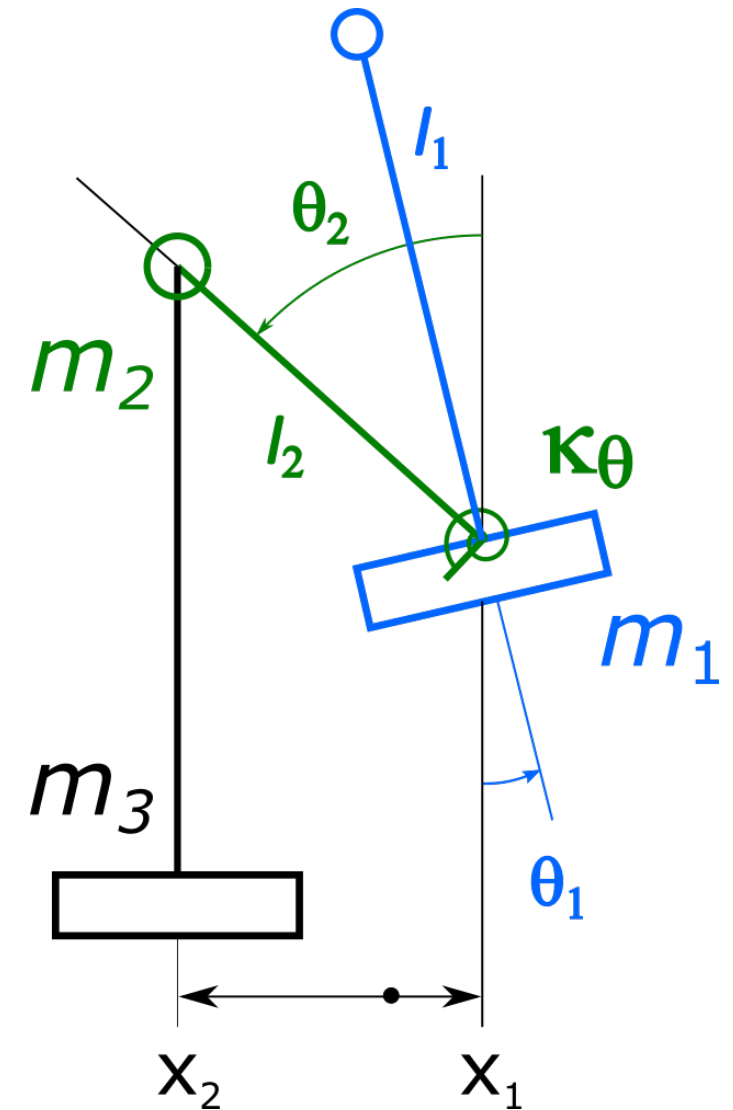
Shortening the path to the test mass



How to soften a suspension stage

- Spare length
- For κ_θ sufficiently stiff, the system is stable
- l_1 : 1.544, # Pendulum length\
- l_2 : 0.520, # IP length\
- T_1 : 2551.0, # Pendulum tension\
- T_2 : 1766.0, # IP compression\
- m_1 : 80.0, # Pendulum mass\
- m_2 : 80.0, # Filter mass\
- m_3 : 100.0, # Load\
- I_{1s} : 20.0, # Pendulum moment of inertia \
- I_{2s} : 0.8, # IP moment of inertia\
- k : 1700.0, # flex joint elastic constant\

Normal mode frequencies
0.68 Hz 0.74 Hz



Horizontal attenuation of a single PIP No damping

$$A = \left(\frac{f_0^2}{f^2 - f_0^2} \right)^2$$

For $f_0 = 0.75$ Hz

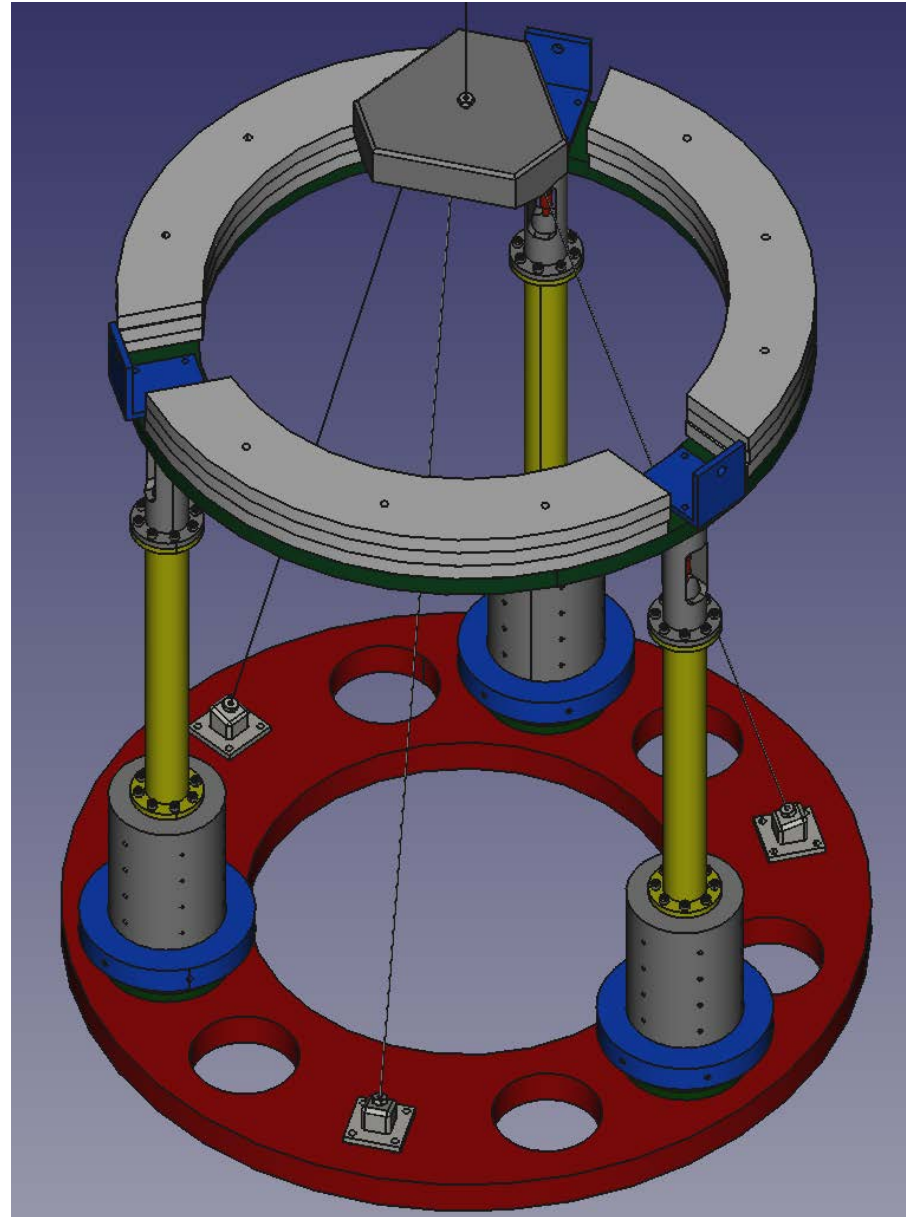
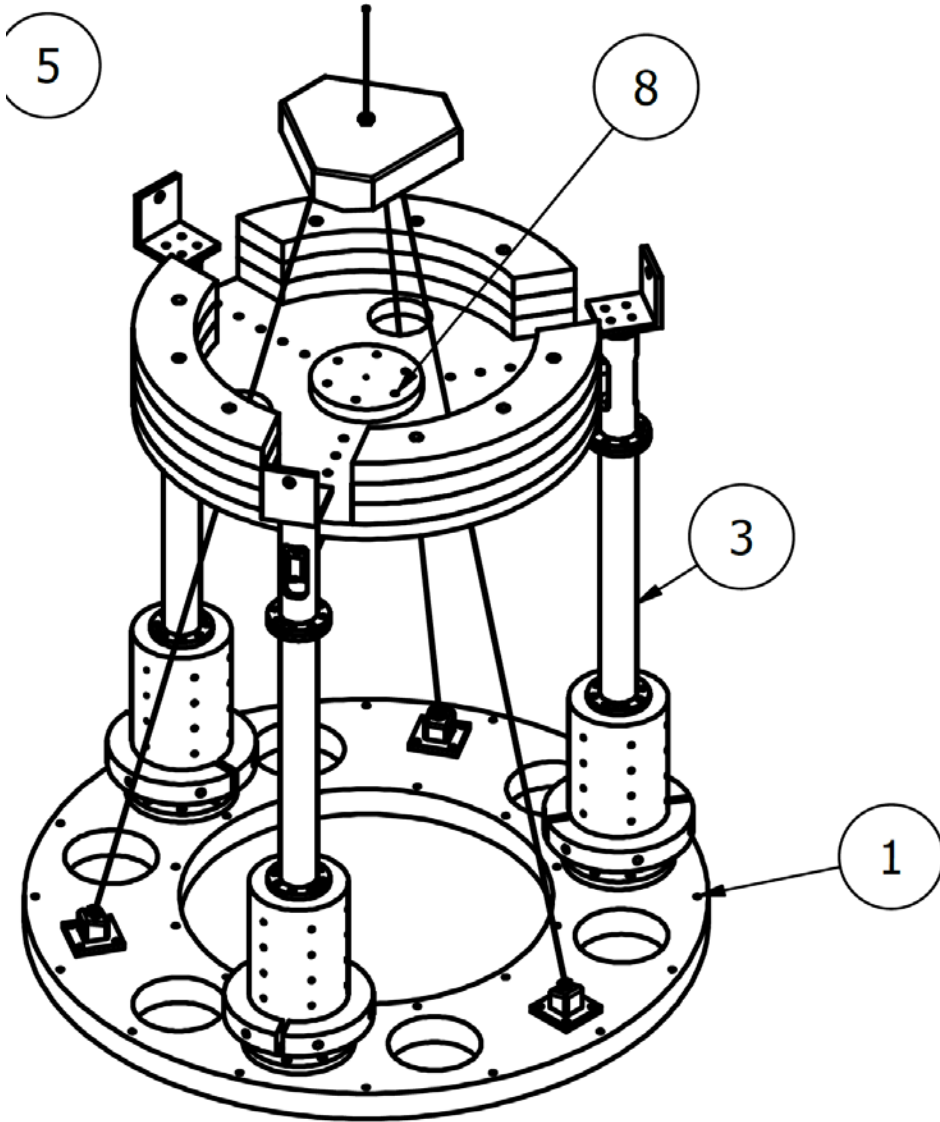
A_2 : attenuation at 2 Hz $2.7 \cdot 10^{-2}$

Two PIP

A_2 : attenuation at 2 Hz $7.2 \cdot 10^{-4}$

Three PIP

A_2 : attenuation at 2 Hz $1.9 \cdot 10^{-5}$



Standard filter addition for vertical attenuation

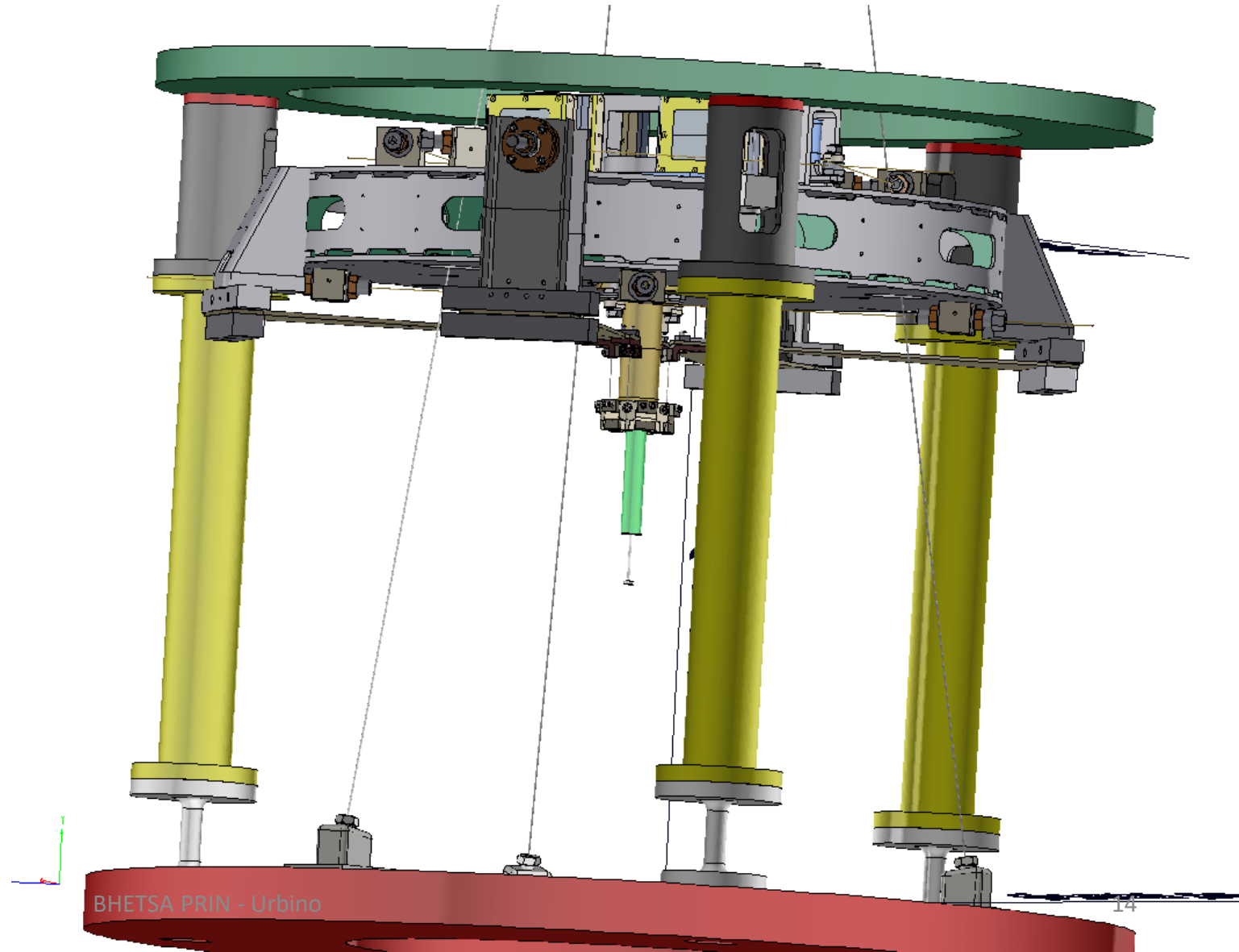
Filter suspended to IP
legs

IP counterweights not
represented

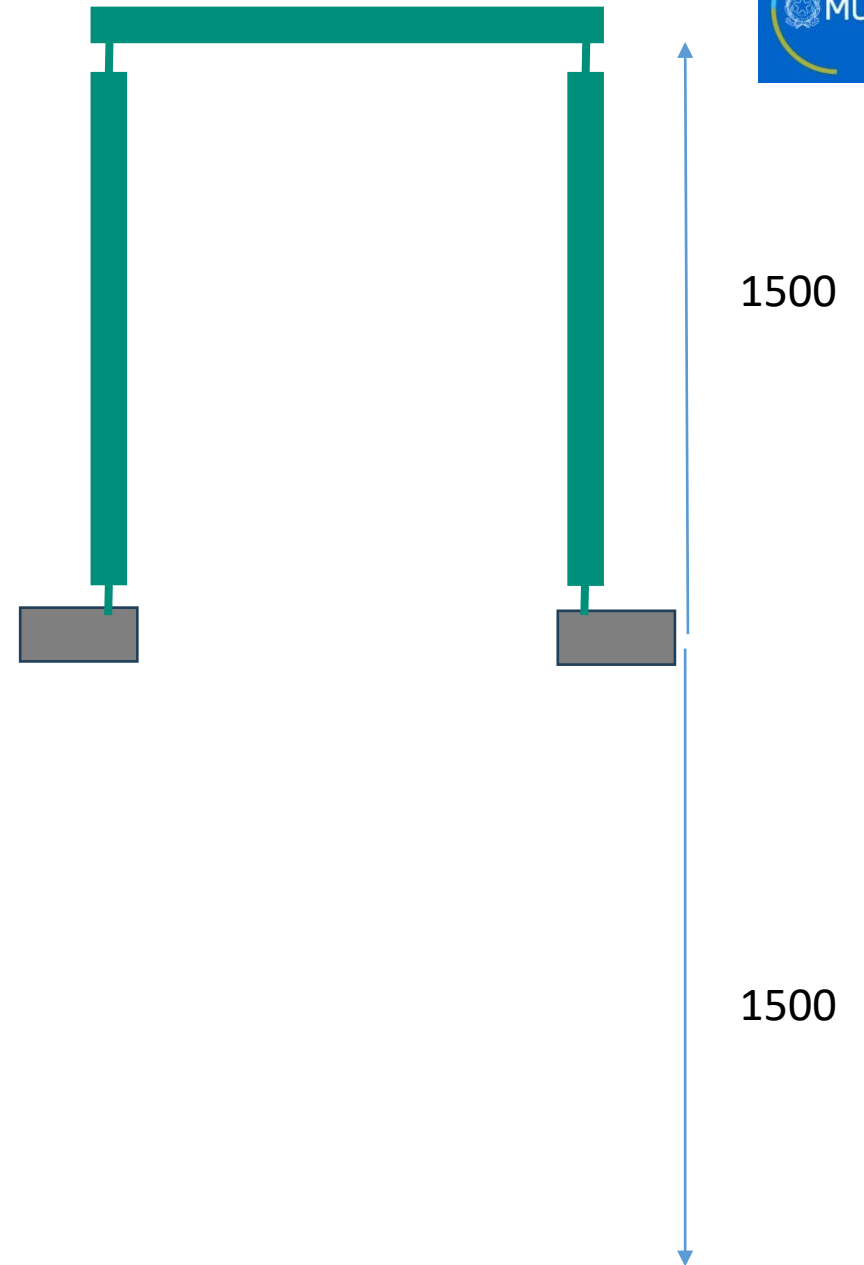
Includes one stage of
vertical attenuation

Hook to next stage
above first pendulum
mass

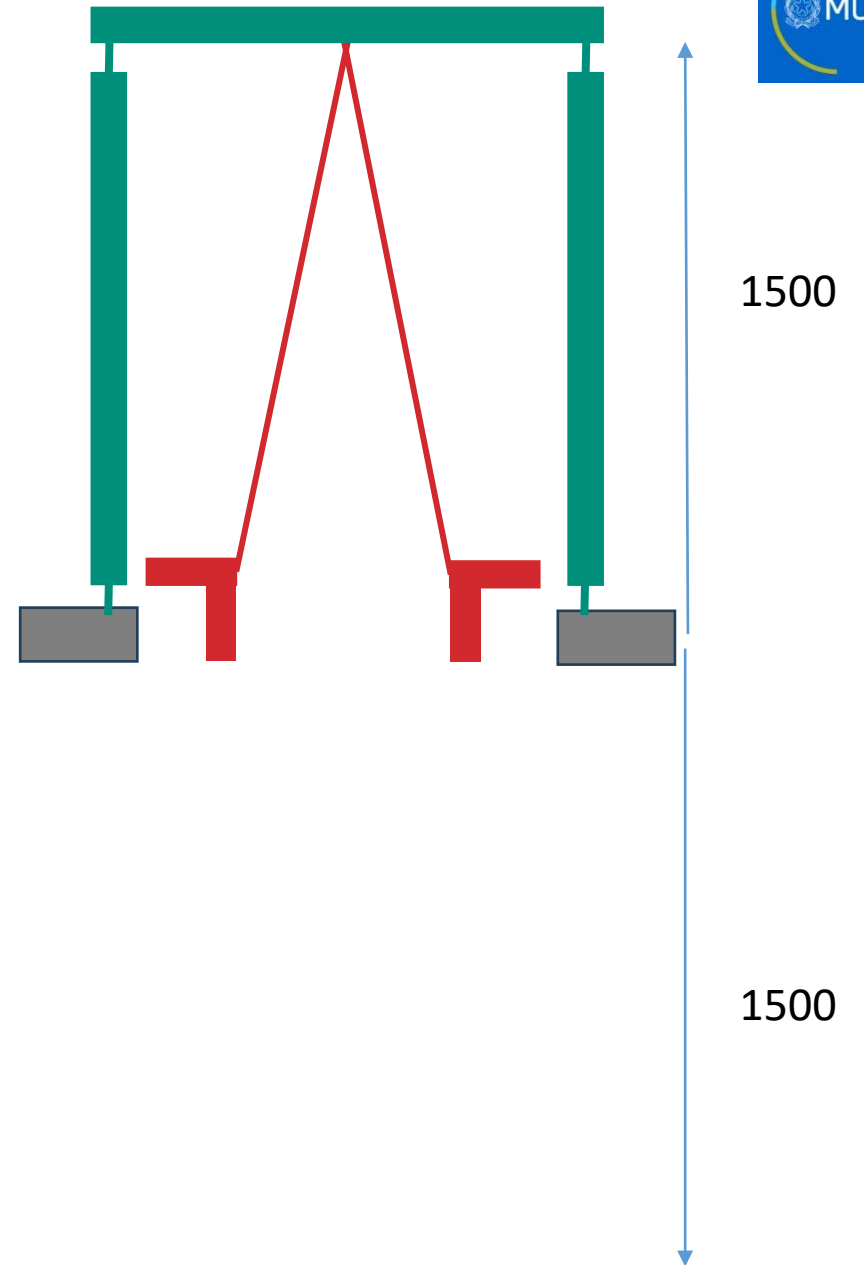
Additional vertical
attenuation can be
suspended below the
filter



- The high part of a suspension chain can be built
 - Starting from an IP

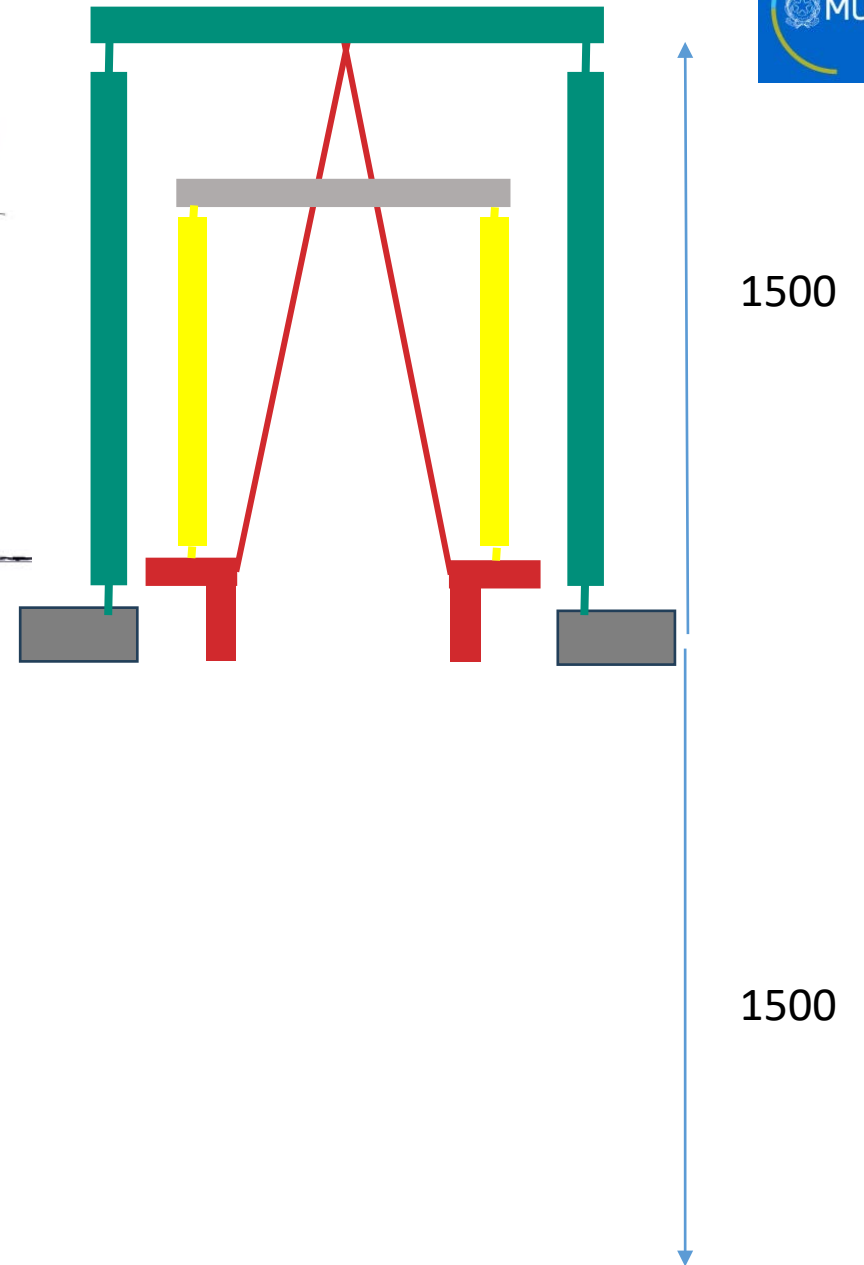
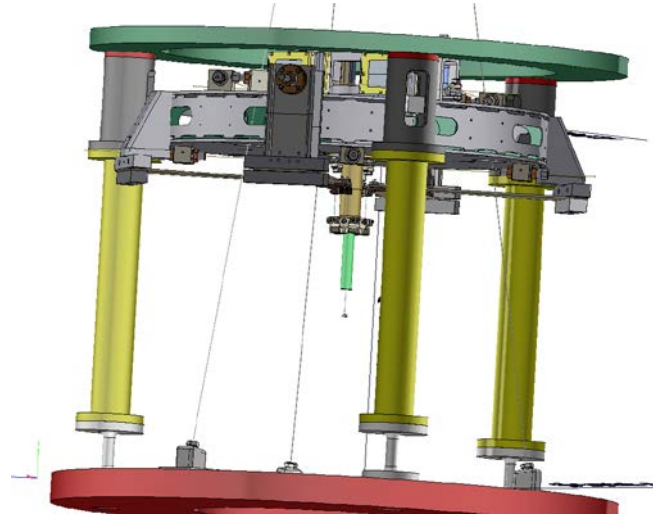


- **The high part of a suspension chain can be built**
 - Starting from an IP
 - Hanging a pendulum



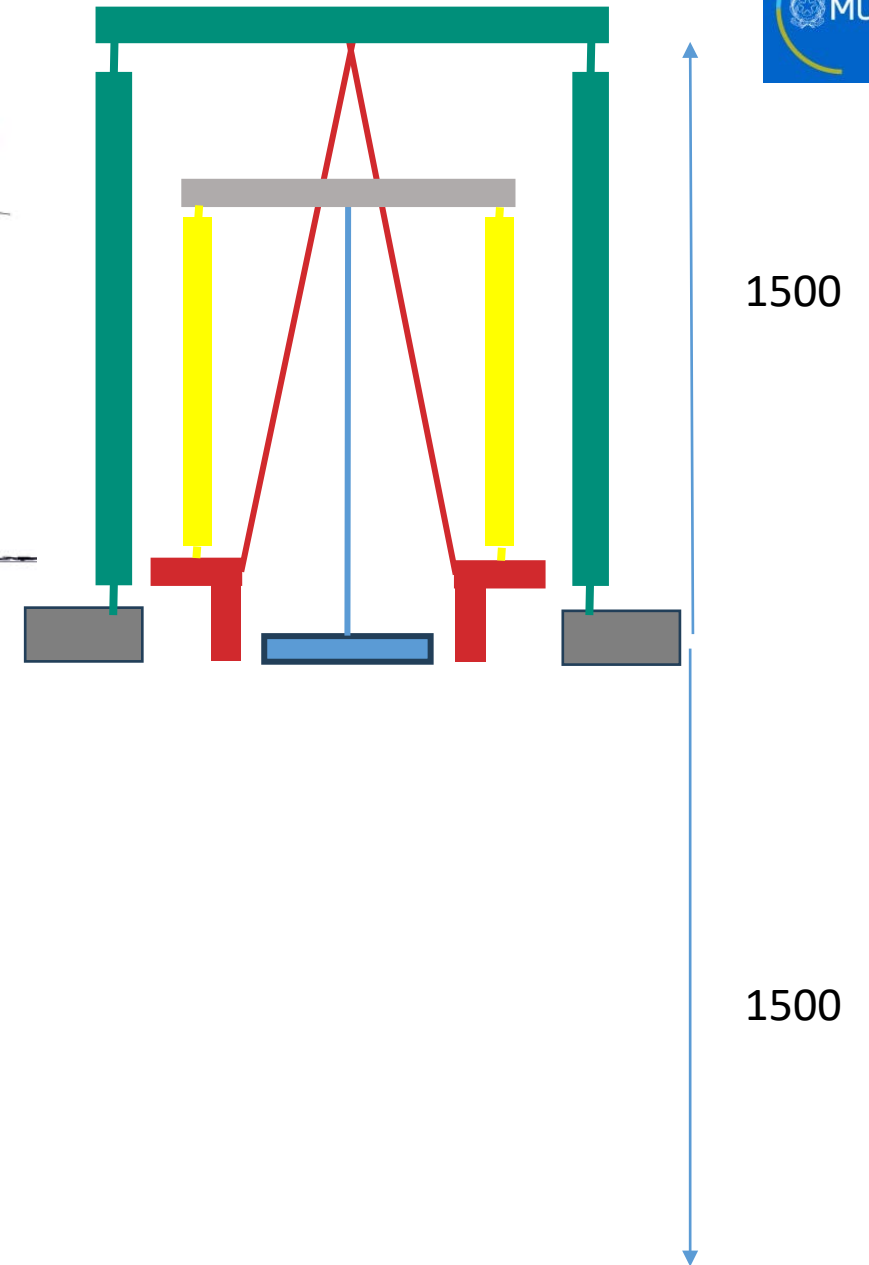
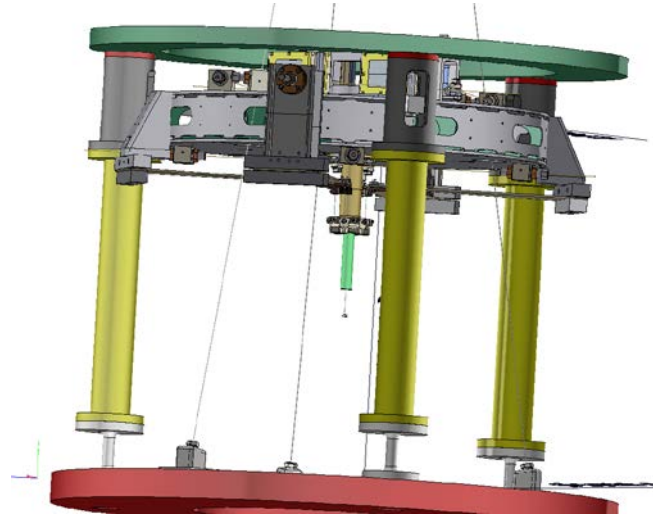
- The high part of a suspension chain can be built

- Starting from an IP
- Hanging a pendulum
- Adding an Inverted Pendulum (-> PIP)



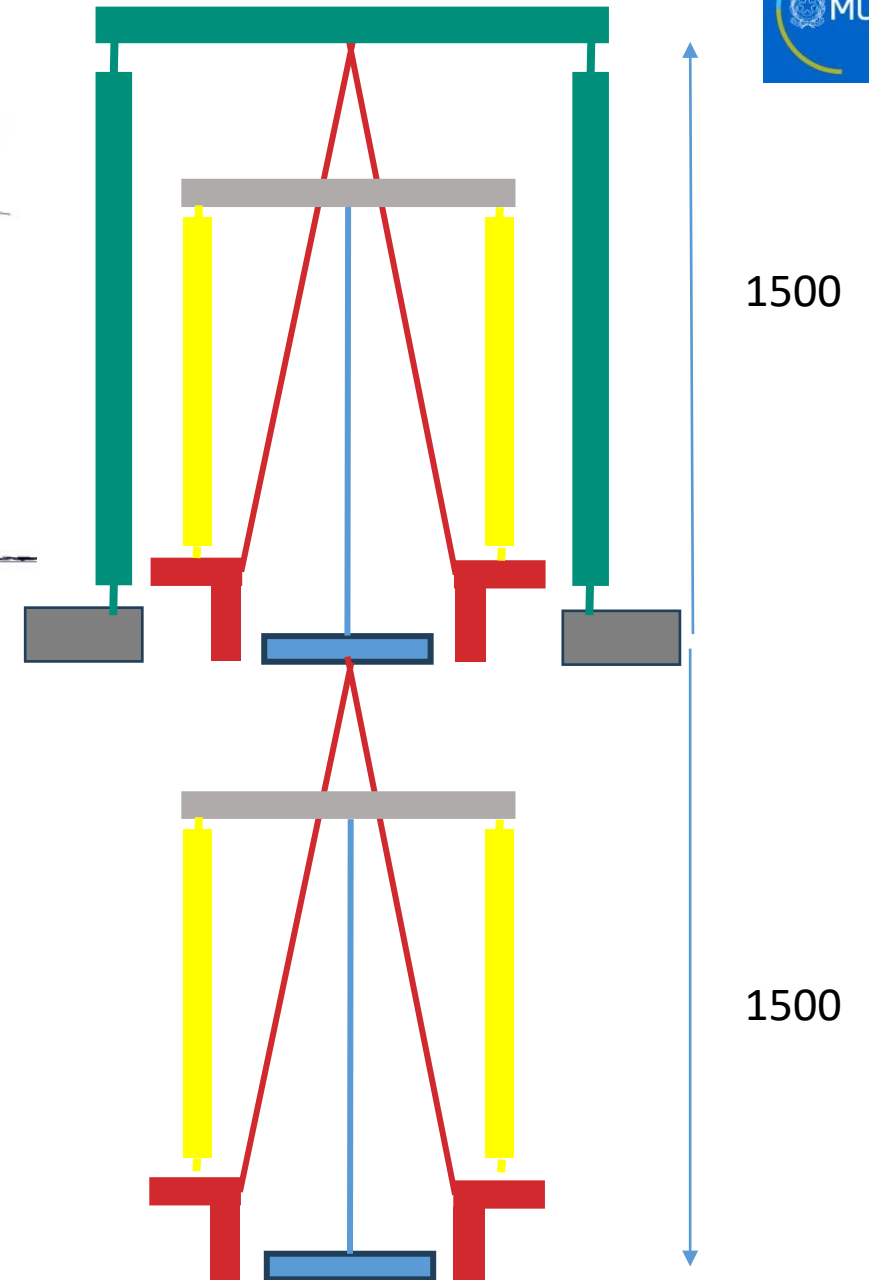
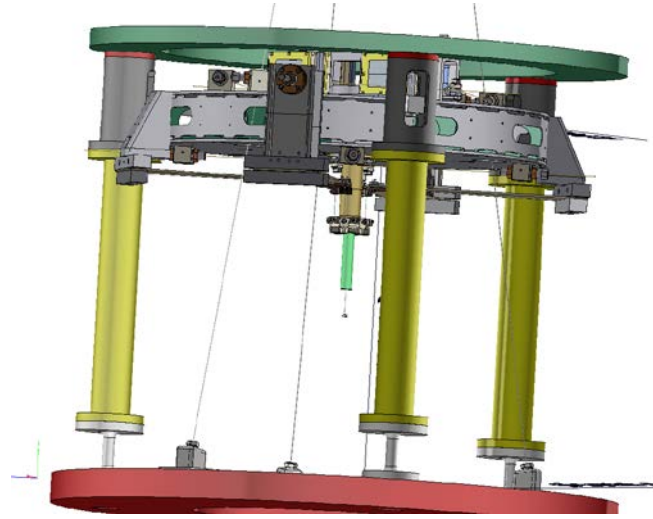
- **The high part of a suspension chain can be built**

- Starting from an IP
- Hanging a pendulum
- Adding an Inverted Pendulum (-> PIP)
- Suspend a vertical isolation filter



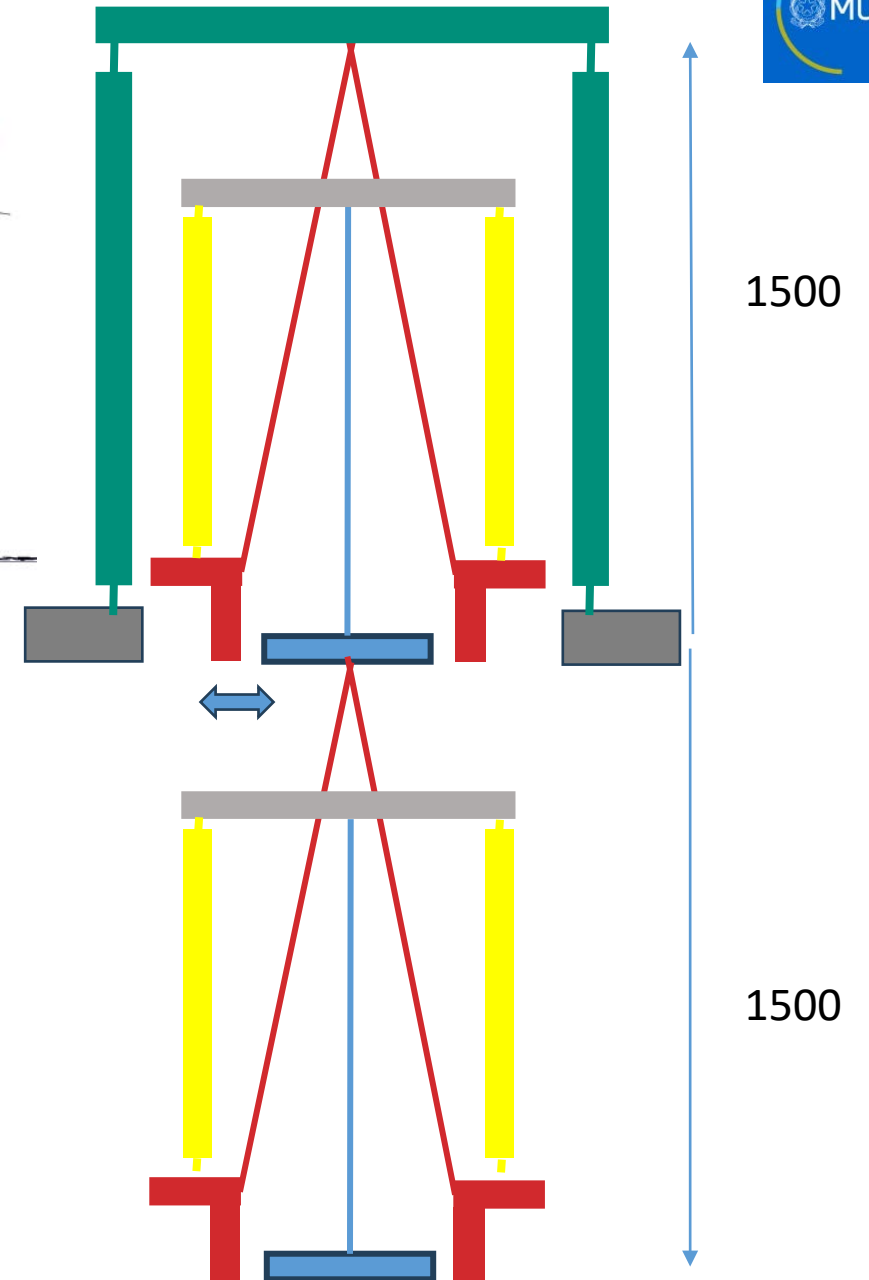
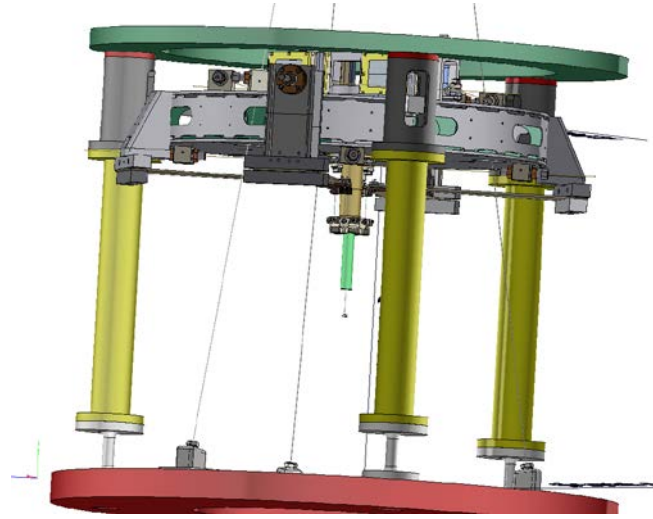
- **The high part of a suspension chain can be built**

- Starting from an IP
- Hanging a pendulum
- Adding an Inverted Pendulum (-> PIP)
- Suspend a vertical isolation filter
- That suspends another PIP



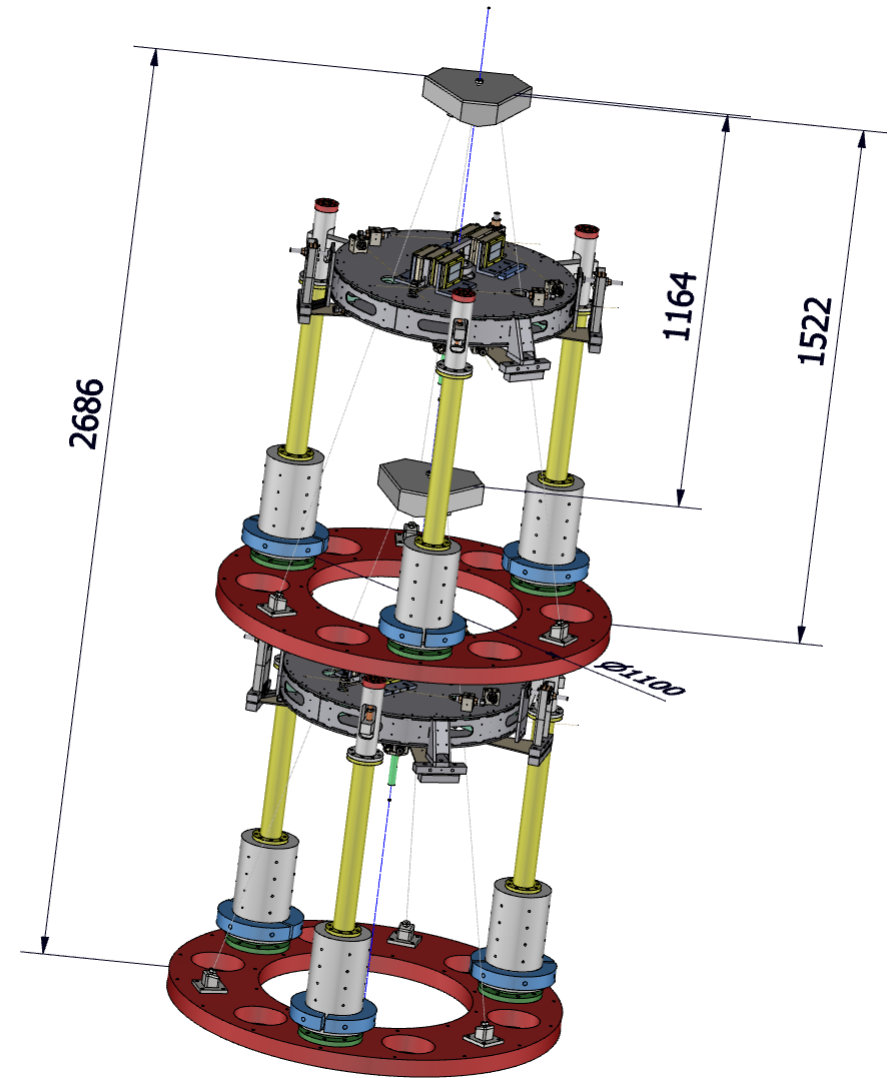
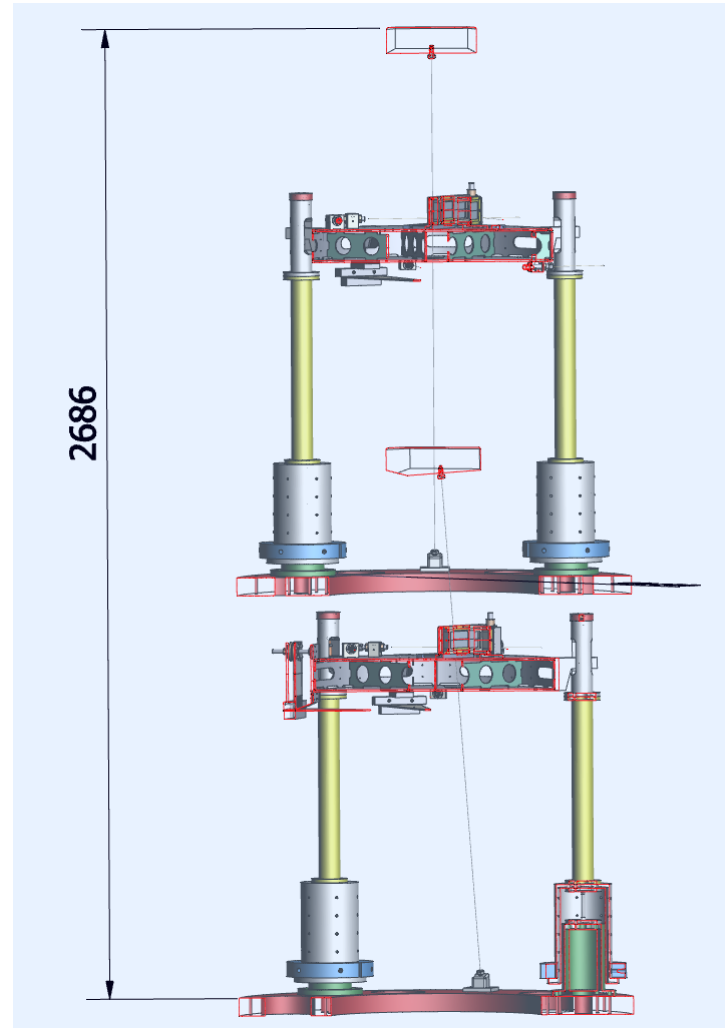
- The high part of a suspension chain can be built

- Starting from an IP
- Hanging a pendulum
- Adding an Inverted Pendulum (-> PIP)
- Suspend a vertical isolation filter
- That suspends another PIP
- Possibility to apply inter-filter feedback



Work in progress
on entangled PIP

Four filters
in 2.70 m



- **A PIP chain can be built**

- Hook of the second PIP above the first filter
- Current PIP length 1.55 m
- Two PIP can live in $2.70 + 0.30 = 3.0$ m accounting for a dedicated vertical attenuation stage
- Three PIP can live in 4 m

- **The goal of a 10 m tall suspension seems in sight**

WP1 A prototype PIP has been manufactured (SarGrav, G&M)

Goals

- Verify the dynamical behaviour: large roll-displacement coupling
- Expected resonances
- Cross coupling
- Vertical bouncing modes

Test of components (see Lorenzo, Sara and Matteo's talks)

WP2 Simulations are in progress (see Max, Matteo's talks)

Modifications on Filter 7 (Andrea Basti)

Laboratory equipment and software support (see Lorenzo and Michele's talk)

WP3 Sensors and actuators

- Tiltmeter progress (Annalisa's talk)
- Develop new accelerometer with better position sensing
- Explore optical readout
- Explore microTCA electronics (Valerio's talk)

WP4 Control and ML (see Gaia and Maria's talks)

WP5 SarGrav (Davide, Domenico)

WP6 Outreach (Davide, Domenico)